

Today: Section 15.3 and 15.4

Next time: Section 16.1

## Instantaneous center of rotation:

L15, p2

Take a rigid body that is in plane motion with a rotation  $\vec{\omega}_A$  about some point A that has velocity  $\vec{v}_A$



For point A we could find some other point C such that  $\vec{v}_A = \vec{\omega}_A \times \vec{r}_{AC}$

Note: since  $\vec{r}_{AC} \cdot \vec{v}_A = \vec{r}_{AC} \cdot (\vec{\omega}_A \times \vec{r}_{AC}) = 0$   
 $\vec{r}_{AC}$  &  $\vec{v}_A$  must be perpendicular.

What about some other point on the rigid body?

Take some point B on the rigid body.



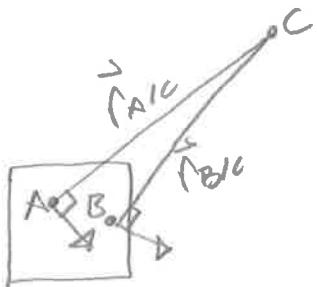
$$\begin{aligned} \text{we have } \vec{v}_A &= \vec{\omega}_A \times \vec{r}_{AC} \text{ & want} \\ \text{to construct } \vec{v}_B: \quad \vec{v}_B &= \vec{v}_{Ba} + \vec{v}_A \\ &= \vec{\omega}_A \times \vec{r}_{Ba} + \vec{\omega}_A \times \vec{r}_{AC} = \vec{\omega}_A \times (\vec{r}_{Ba} + \vec{r}_{AC}) \\ &= \vec{\omega}_A \times (\vec{r}_B - \vec{r}_A + \vec{r}_A - \vec{r}_C) = \vec{\omega}_A \times (\vec{r}_B - \vec{r}_C) \\ &= \vec{\omega}_A \times \vec{r}_{BC} \end{aligned}$$

We now have  $\vec{v}_B$  constructed as a rotation about point C. Since B was arbitrary, this works for all points on the rigid body!

For this one instance in time we have a single center of rotation for all points on the rigid body.

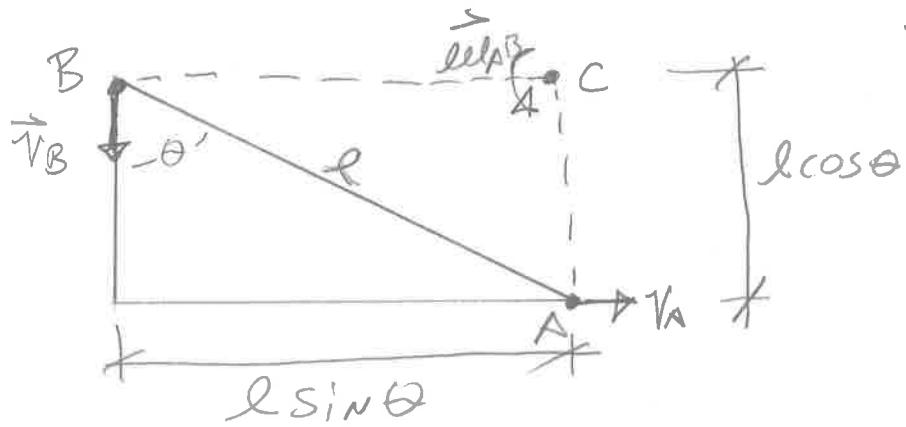
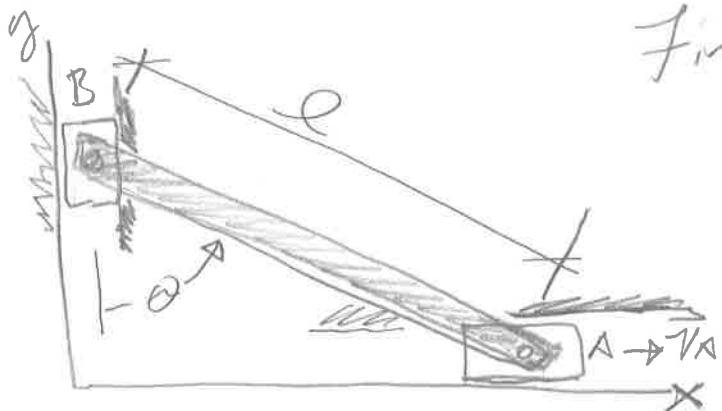
L15, p3

As with point A, the velocity of point B is perpendicular to the line connecting it to point C



Example: Given  $\vec{v}_A = v_A \hat{x}$ ,  $l$  &  $\theta$

Find  $\vec{v}_B$  &  $\vec{v}_{AB}$



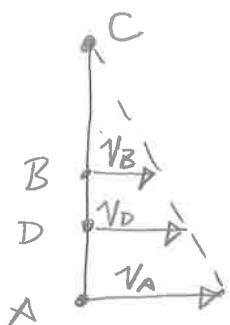
$$\begin{aligned} v_B &= l \omega_B l \cos \theta \\ \Rightarrow \vec{v}_{AB} &= \left( \frac{v_A}{l \cos \theta} \right) \hat{\imath} \\ \text{And } \vec{v}_B &= \omega_B l l \sin \theta \hat{\jmath} \\ &= \left( \frac{v_A}{l \cos \theta} \right) l \sin \theta \hat{\jmath} \\ &= v_{A \tan \theta} \hat{\jmath} \end{aligned}$$

This method for this problem is easier to solve than our previous method.

L15, p4

For every point P on the rigid body (in plane motion that is rotating)  $\vec{v}_P = \text{ell} \vec{r}_{PC}$

Here ell is fixed  $\Rightarrow \vec{v}_P$  scales with  $r_{PC}$



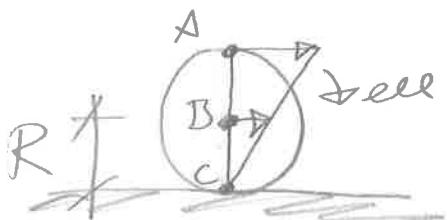
If point B is  $\frac{1}{2}$  distance from C as is A, then  $v_B = \frac{1}{2}v_A$ .

If point D is  $\frac{3}{4}$  distance from C as is A, then  $v_D = \frac{3}{4}v_A$   
And on & on.

This forms similar triangles  $\Rightarrow \frac{v_B}{r_{BC}} = \frac{v_D}{r_{DC}} = \frac{v_A}{r_{AC}}$

Wheel rolling w/o slipping: We know that

$$v_A = 2v_B \quad \& \quad v_c = 0$$



In fact, we now know that point C is the instantaneous center of rotation.

S15.4

Relative motion for two points:

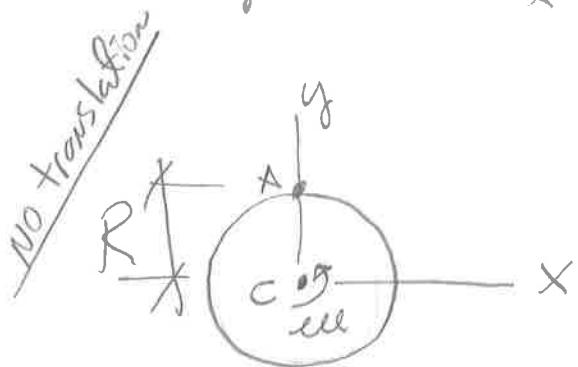
$$\vec{r}_{AB} = \vec{r}_A - \vec{r}_B \Rightarrow \vec{r}_A = \vec{r}_{AB} + \vec{r}_B \quad \& \quad \vec{v} = \frac{d\vec{r}}{dt} \Rightarrow \vec{v}_A = \vec{v}_{AB} + \vec{v}_B$$

For a rigid body, the distance between A & B is fixed  $\Rightarrow \vec{r}_{AB}$  is purely rotational so  $\vec{v}_{AB} = \text{ell} \times \vec{r}_{AB}$

Acceleration  $\vec{a} = \frac{d\vec{v}}{dt} \Rightarrow \vec{a}_A = \vec{a}_{AB} + \vec{a}_B$  where

$$\vec{a}_{AB} = \vec{\alpha} \times \vec{r}_{AB} + \text{ell} \times [\text{ell} \times \vec{r}_{AB}]$$

In the past we used  $\vec{a} = \omega \hat{e}_n + \alpha \hat{e}_t$  for circular motion. How does this relate to our new expression?



$$\vec{e}_{\parallel} = e_{\parallel} \hat{e}_z \text{ with } e_{\parallel} = \text{constant}$$

$$\vec{a}_n = \omega \hat{e}_n + \alpha \hat{e}_t, \text{ where}$$

$$\omega_n = \frac{V_A}{R} \text{ & } \alpha_t = \frac{dV_A}{dt}$$

$\hat{e}_n$  points from A to C and  $\hat{e}_t$  is tangential to the path that A takes.

For uniform circular motion  $V_A = R e_{\parallel}$  &  $\frac{dV_A}{dt} = \alpha$  so  $\omega_n = R e_{\parallel}$  &  $\alpha_t = \alpha$  &  $\hat{e}_n = -\hat{j}$  so

$$\vec{a}_{AIC} = \vec{a}_n = R e_{\parallel}^2 (-\hat{j})$$

But if  $e_{\parallel}$  constant we get

$$\frac{dV}{dt} = R \frac{de_{\parallel}}{dt} = R \alpha \text{ and } \hat{e}_t = -\hat{x} \text{ now}$$

$$\vec{a}_{AIC} = \vec{a}_n = \alpha R (-\hat{x}) + R e_{\parallel}^2 (-\hat{j})$$

Our expression  $\vec{a}_{AIC} = \alpha R (-\hat{x}) + R e_{\parallel}^2 (-\hat{j})$  has to match what we would get using

$$\vec{a}_{AIC} = \vec{\alpha} \times \vec{r}_{AIC} + \vec{e}_{\parallel} \times [\vec{e}_{\parallel} \times \vec{r}_{AIC}] \text{. Here } \vec{\alpha} = \alpha \hat{z} \text{ & } \vec{e}_{\parallel} = e_{\parallel} \hat{z}$$

$$\text{ & } \vec{r}_{AIC} = R \hat{j} \text{ so } \vec{a}_{AIC} = \alpha R (\hat{z} \times \hat{j}) + e_{\parallel}^2 R \hat{z} \times [\hat{z} \times \hat{j}]$$

$$\text{But } \hat{z} \times \hat{j} = -\hat{x} \text{ & } \hat{z} \times (-\hat{x}) = -\hat{j} \text{ so } \vec{a}_{AIC} = \alpha R (-\hat{x}) + e_{\parallel}^2 R \hat{z} \times (-\hat{x})$$

$$\Rightarrow \vec{a}_{AIC} = \alpha R (-\hat{x}) + e_{\parallel}^2 R (-\hat{j}) \text{ This matches previous expression } \odot$$

Example: Wheel rolling with no

L15, pg

slipping

$$\vec{a}_A = \vec{a}_{A/C} + \vec{a}_C \quad \text{If } \dot{v}_c = \text{const.}$$

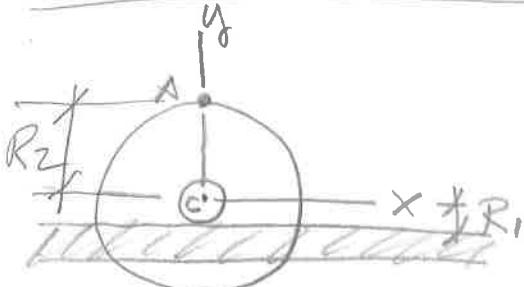
$$\text{then } \vec{a}_c = \vec{\omega} \quad \text{if } \vec{\alpha} = \vec{\omega} \quad \text{if } v_c = R\omega$$

$$\text{so } \vec{a}_A = R\omega^2(-\hat{y})$$

$$\text{If } \dot{v}_c \neq \text{const} \text{ then } \vec{\alpha} \neq \vec{\omega} \text{ and } \vec{a}_c \neq 0$$

$$\Rightarrow \vec{a}_A = \alpha R(-\hat{x}) + \omega^2 R(-\hat{y}) + \vec{a}_c$$

Example: Flywheel on shaft rolling on rail



Given  $v_c, \alpha_c, R_1 \& R_2$  find  $\vec{a}_A$ :

$$\vec{a}_A = \vec{a}_{A/C} + \vec{a}_C$$

$$\text{where } \vec{a}_{A/C} = \vec{\alpha} \times \vec{r}_{A/C} + \vec{\omega} \times [\vec{\omega} \times \vec{r}_{A/C}]$$

$$\dot{v}_c = v_c \hat{x} = R_1 \omega \hat{x} \quad \text{so} \quad \vec{\alpha} = (v_c/R_1)(-\hat{z})$$

$$\text{and } \vec{a}_c = \alpha_c \hat{x} = R_1 \alpha \hat{x} \quad \text{so} \quad \vec{\omega} = (\alpha_c/R_1)(-\hat{z})$$

Note: Assumed wheel is moving in +x-direction.

If wheel is moving in negative x-direction, then  
 $v_c \rightarrow$  Negative and sign of  $\vec{\alpha}$  is still good

We also have  $\vec{r}_{A/C} = R_2 \hat{y}$  so  $\vec{a}_A = \vec{a}_{A/C} + \vec{a}_c$

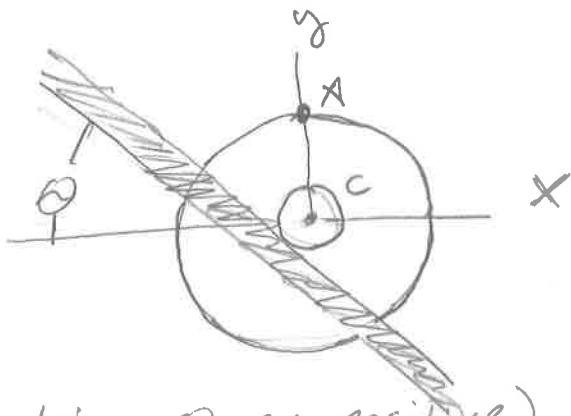
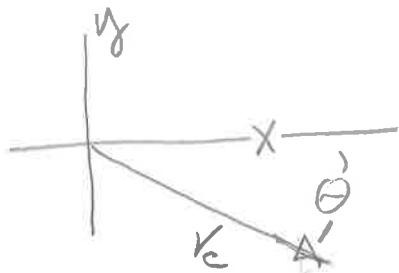
$$\Rightarrow \vec{a}_A = \frac{\alpha_c}{R_1} R_2 (-\hat{z}) \times \hat{y} + \frac{v_c^2}{R_1^2} R_2 \hat{z} \times [\hat{z} \times \hat{y}] + \vec{a}_c$$

$$\Rightarrow \vec{a}_A = \left( \frac{\alpha_c R_2}{R_1} \right) \hat{x} + \alpha_c \hat{x} + \left( \frac{v_c^2 R_2}{R_1^2} \right) (-\hat{y})$$

L15, p7

Note: In this case  $\vec{a}_c = a_c \hat{x}$

If rail was tilted some angle  $\theta$  with respect to horizontal then



$$\vec{v}_c = v_c \cos \theta \hat{x} - v_c \sin \theta \hat{y} \quad (\text{taking } \theta \text{ as positive})$$

Note: if we took  $\theta$  as negative then

$$\vec{v}_c = v_c \cos \theta \hat{x} + v_c \sin \theta \hat{y} \quad \text{Just have to be consistent with sign convention.}$$

Also (keeping  $\theta > 0$ )

$$\vec{a}_c = a_c \cos \theta \hat{x} - a_c \sin \theta \hat{y}$$

Now

$$\vec{a}_A = \left[ \frac{a_c R_2}{R_1} \hat{x} + a_c \cos \theta \hat{x} \right] + \left[ \left( \frac{v_c^2}{R_1^2 R_2} \right) (-\hat{y}) + a_c \sin \theta \hat{y} \right]$$